

Gasket and Sealing Technologies Pvt. Ltd.

Gaskets at a Glance

Gasket and Sealing Technologies Pvt. Ltd.

Introduction

Gasket and Sealing Technologies Pvt. Ltd. is a leading manufacturer of precision-engineered gaskets, seals, and related products for diverse industrial applications. Our focus is on developing and delivering superior-quality products that offer excellent performance and reliability, helping our customers achieve optimal efficiency and productivity. Our flagship brand, Macer, represents our commitment to excellence and innovation in gasket manufacturing.

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About Us

At Gasket and Sealing Technologies Pvt. Ltd., we are a leading manufacturer of high-quality spiral wound gaskets, Kammprofile Gaskets, Jacketed Gaskets, Fibre Gaskets specializing in providing reliable sealing solutions for a wide range of industries. With our dedication to quality, innovation, and customer satisfaction, we have established ourselves as a trusted name in the gasket manufacturing industry. Our promoters have over 50 years of experience in this particular industry. Over the past 5 decades with our hard work and commitment we have served various industries in their sealing solutions. After understanding the industry and catching the emotions of the client we decided to launch our brand MACER with only one purpose in mind, we will provide quality products at the most affordable price.

We take pride in our ISO 9001:2015 certification, a testament to our unwavering dedication to quality management systems. This internationally recognized certification demonstrates our commitment to delivering exceptional products and services consistently.

Our Vision

Our vision is to be a world-class provider of sealing solutions, setting new standards for quality, performance, and customer service. We strive to continuously improve our products and processes, exceed customer expectations, and contribute to the success of our clients by delivering exceptional sealing solutions that ensure operational efficiency and reliability.

Our Mission

Our mission is to design, manufacture, and supply gaskets of superior quality, precision, and durability. We aim to be at the forefront of technological advancements in the gasket industry. constantly innovating and adapting to meet the evolving needs of our customers. Through our commitment to excellence, we aim to build long-lasting partnerships with our clients, providing them with the highest level of service and support.

We are dedicated to:

- **Quality:** We adhere to stringent quality control measures throughout the manufacturing process to ensure that our gaskets meet the highest industry standards. We utilize advanced technologies and employ skilled professionals to deliver products of uncompromising quality.
- Innovation : We embrace innovation and invest in research and development to stay ahead of industry trends. By leveraging the latest technologies and materials, we continually improve our proucts to meet the ever-changing demands of our customers.
- Customer Satisfaction : Customer satisfaction is at the heart of everything we do. We prioritize understanding our customers' needs, providing personalized solutions, and delivering products on time, every time. We aim to build strong, long-term relationships with our clients based on trust, reliability, and mutual success.
- Sustainability: We are committed to conducting our business in an environmentally responsible manner. We strive to minimize our ecological footprint by implementing sustainable practices, reducing waste generation, and optimizing energy efficiency in our operations.

With our company, Gasket and Sealing Technologies Pvt. Ltd., and our brand, Macer, you can trust that you are partnering with a reputable and forward-thinking organization that is dedicated to providing exceptional sealing solutions. We look forward to serving you and contributing to your success with our high-quality gaskets

MACER[®] takes great pride in having achieved universal acceptance for providing gaskets used in sealing applications where extreme mechanical and thermal performance demands are considered routine.

There are many companies in the sealing industry. Very few can boast the quality of products, quality of service and quality of people found at **MACER®**.

Introduction

For years, many different types of gasket have been used to seal bolted connections. Few people in industry give them much thought until problems arise. This document is intended to promote a clearer understanding of how gaskets work, and how to avoid common pitfalls in their use. Let us first define what a gasket is - imagine writing a technical dictionary and needing to define what a gasket is or does. One might simply suggest that it is something for sealing flanges on pipe-work or process equipment. The **MACER[®]** definition should help the reader to picture how the gasket functions.

Thus the gasket has to react to the forces generated by the bolts, and therefore the work and energy imparted to the bolted joint becomes 'stored' within the gasket itself. Gaskets can be classified into three main categories:

\leftrightarrow Non-Metallic

(Elastomers, Cork, Compressed Fibre, Graphite, PTFE etc.)

Semi-Metallic

(Spiral-Wound, Clad Joints, Kammprofile, etc.)

Metallic

(API Ring Joints, Lens Rings etc.)

energy between them."

storing

surfaces, by

Each has its own advantages, and the semi-metallic & metallic will be described further in this manual. The maximum service conditions (operating pressure for example) for semi-metallic gaskets will be higher than for non-metallic, and fully metallic joints are likely to be used at even higher operating conditions. "A device for sealing two

Bolted Joint Assemblies

There are two main types of bolted joint assembly, which can be considered to be 'floating' and 'rigid' in their basic characteristics. A 'floating' assembly is one where there is no metal to metal contact after bolting the flanges. This would be the commonly encountered raised face flange having a fibre-based material gasket. Here, for an increase in system pressure a higher gasket stress would be required. However, with increasing bolt force the gasket undergoes greater compression.Additionally the bending moment on the flanges is increased, so that the bolts, flanges and gasket could all be considered to be 'spring elements' within the system (though the gasket is often a highly nonlinear element in its load-recovery behaviour). A 'rigid' assembly, is where metal to metal contact occurs after bolting. An example of a 'rigid' assembly can be illustrated by an O-ring in a recess. Once the flanges have achieved a metal-to-metal contact, then further tightening of the bolts against the system pressure has no further effect upon the sealing element. As an O-ring is self-energising, then the degree of sealing should be good, provided no extrusion gap exists between the flanges.

तत ÜП **FLOATING RIGID ASSEMBLY ASSEMBLY**

The initial boltload generated upon tightening is transferred to the gasket via the flanges. This initial seating stress compresses the gasket and tightens it within itself. The hydrostatic forcegenerated by the system pressure, tends to 'unload' and reduce the stress on the gasket. The stress remaining on the gasket is considered to be the 'operating' or'residual' stress. It is this degree of stress, or energy left in the joint that will

determine the degree of tightness achieved in the system.It should be noted that on a raised face assembly such as the one shown here, there will be some deflection of the flanges themselves ('flange' 'rotation'). This is a function of the load applied, the flange material and the geometry of the flanges. Thus, the operational stress towards the outside edge of the gasket tends to be greater than on the inside edge. The mechanics concerning flange rotation are altered with flat-faced flanges. The overall contact area of a full-face joint can be typically twice as much as an inside bolt circle (IBC gasket).

Gasket Behaviour

Section 2

Stress Relaxation (a

The stress relaxation performance or the stress retention property of a gasket is vital in maintaining the level of energy stored in the joint, which effects the seal. Relaxation can occur at the flange-gasket interface as well as within the gasket material itself. This characteristic is particularly relevant in relation to non-metallic sheet jointing materials, where there are internationally recognised test procedures for examining relaxation effects. These involve stressing the gasket to a pre-determined amount and subjecting it to elevated temperatures for a given time (16 hours at 3000C for example). At the end of the test the remaining stress level is measured, where materials giving the higher readings are generally considered to be more successful. Materials having a high rubber/elastomer content for example, may be expected to relax significantly as the rubber/elastomer decays at temperature. It should be well noted that for fibre sheet jointing materials, that thick materials exhibit increased relaxation over thin ones. Thus, the thinnest gasket possible should always be used, and need only be sufficiently thick to take up any flange distortion and misalignment.

Tensile Strength (6)

Tensile strength is not necessarily the most important function of a gasket material. Expanded graphite for example is relatively weak, though it performs very well as a gasket material, with a high degree of sealability in a wide range of media. If a aasket is adeauately loaded on a flange with the correct surface finish, then the clamping forces resist the tendency for the joint to 'blow-out' at pressure. However, if the joint is relatively thick (i.e. with a significant area exposed to the system pressure) and inadequately compressed, then the internal pressure forces on the inside edge have to be resisted by the tensile strength of the gasket. Again, the thinner the gasket the less relaxation will occur internally as well as exposing less area to the system pressure that is trying to force the gasket from between the flanges.

C **Effect of Flange Surface Finish**

Normally, standard piping flanges are supplied with a light gramophone-finish groove across the gasket seating face (see following table for typical values) These values are suitable for non-metallic and semi-metallic gaskets, whereas values for metallic gaskets are specified within relevant international standards, e.g. API 6A for ring joint gaskets. This finish tends to 'grip' the gasket material and thereby limits the creep across the flange faces. Note that the surface finish should not be so rough as to allow a leak path under the gasket, where the gasket is unable to deform effectively to fill the gramophone groove. The use of pastes on the gasket surface may actually worsen sealing performance as these can fill-in the surface finish allowing stress relaxation to occur. Any flange damage (e.g. steam cutting, etc.) should be rectified before a joint is re-made. The spirally grooved, "gramophone" surface finishes as specified in common flange standards such as BS 1560, generally provide a good surface for most gasket types. These usually recommend that the flange faces be machined with a spiral groove in accordance with the table below. Individual attention should be given to applications involving searching gases or high vacuum sealing. As a general rule we prefer flange finishes of between 3.2 and 6.3µm Ra as being the recommended surface for use with spiral-wound gaskets, and 6.3 to 12.5µm Ra for compressed fibre materials, though both types should give acceptable performance over the complete range of finish shown. Note: Wherever possible, the mating flanges should be of the same material and machined identically. It is also important that the flange surfaces are flat, free of imperfections, and as far as practicable are parallel.

C Load-Sealability

It is a fact that all gaskets leak to varying degrees. For example, whilst an assembly may be built and hydro-tested successfully, if it were pressurised with helium for example and the flange encapsulated, it may be possible to detect a small mass-leak rate of the helium, after a period of time, using a mass-spectrometer. This leak-rate might otherwise be considered undetectable in general industrial terms, though the load-sealability tests that are conducted by gasket manufacturers and research bodies are invaluable when looking at critical sealing applications.

A curve of the load-compression characteristics will be very similar, again showing how the material densifies under increasing stress α s any micro-porosity is closed within the material structure. The gasket becomes increasingly hard to compress with increasing applied stress. Most gasket sealing tests are done on α loading-unloading cycle to see the effects of leakage as the gasket stress is reduced (by the hydrostatic force for example), after being loaded to a higher value. It is usually better to create a log-linear plot of the load sealability results. If this is done, then a reasonably straight line is produced as per the example adjacent:

We must assume that in the free, uncompressed state, that a non-metallic gasket may have some internal porosity, as when manufactured, the material may not be perfectly homogenous. Thus, any micro porosity holes in the structure will allow leakage until the applied seating stress causes them to close.

As the gasket densifies under load, such porosity becomes increasingly less and the joint continues to tighten becoming progressively more dense. Therefore, a load leakage test on a gasket will tend to produce an exponential-decay curve format thus.

Note from this graph that as the gasket densifies, then the slope of the data lines changes. Thus, the sealing properties are quite complex, depending upon the initial and operational stress levels that are likely to occur in service. Note that flange rotation effects will further complicate the theoretical stress levels upon the gasket element.

For a given operating stress on a gasket, the leak-rate will increase with increasing system pressure, as indicated in the graph adjacent:

Similarly, for a sheet gasket material, the leak-rate increases with material thickness, roughly in a proportional manner, (i.e. double the gasket thickness produces double the leak rate).

Flange Types & Standards

Flange standards

There are many common flange standards available, though perhaps the most widely used are ASME, DIN and BS. There are of course a large number of other national standards in all countries around the world, though many have their origins in the ASME or DIN series flanges.

There are a wide variety of flange styles, configurations and applicable standards as shown herewith, though in general industry the raised face flange is perhaps the most common type regularly employed.

g i **ASME**

The ASME B16.5 flanges are in widespread use all around the world on power stations, refineries, chemical plants and most other major industrial facilities. This standard covers flanges from 1/2" to 24" nominal bore, which are classified in pressure ratings in pounds per square inch (p.s.i.), such as classes 150, 300, 600, 900, 1500, and 2500. Note that these are pressure ratings at elevated temperatures, as for example a class 150 flange is rated to 290 p.s.i. (20 bar) at ambient.

Large diameter ASME flanges (above 24" and up to 60" N.B.) are covered by the ASME B16.47 standard. This has two main categories - Series A and Series B. The Series A covers flanges formerly known as MSS-SP44 (Manufacturers Standardization Society) whereas Series B covers those from API 605 (American Petroleum Institute), which tend to be more compact. There are other large diameter flange standards such as the Taylor Forge classes 175 and 350, as well as the American Water Works Association (AWWA) flanges.

Heat exchangers are commonly produced having male & female flanges of class 150, 300, or 600 etc., but (Tubular manufactured to **TEMA** Equipment Manufacturers Association) dimensions

O DIN

By comparison to the ASME flanges, the DIN series are rated with PN numbers which indicate the nominal pressure rating in bar. These for example are PN 6, PN10, PN16, PN25, and PN 40 where, unlike the ASME flanges, the pressure ratings relate to ambient temperature. This metric series of flanges are now covered by pan European standards such as EN1092, for these PN rated flanges.

The BS10 flange standard is rarely used, though of course many of these flanges still remain in service at a large number of industrial sites. These flanges are classified by a letter system, for example Table E, Table H, Table J etc. in increasing order of service pressure rating.

C Relevant Gasket Standards

For ASME flanges, then cut gaskets from non-metallic sheet materials, are covered by ASME B16.21 or BS EN 12560 part 1 (formerly BS7076 pt.1). Spiral wound joints for these are made in accordance with ASME B16.20 (formerly to API 601), or to BS 3381 or BS EN 12560 part 2. The ASME B16.20 standard also covers metal jacketed gaskets and API ring joints. For DIN series flanges, gaskets are cut from sheet materials in accordance with EN 1514 part I, with spiral wound joints being made to EN 1514 part 2. The BS EN 12560 and BS EN 1514 have additional sections covering other gasket types such as PTFE envelopes and corrugated metallic gaskets in parts 3 and 4 respectively. As for BS 10 flanges, the cut gasket dimensions are given in BS 3063. In terms of gasket material testing standards, then compressed sheet materials are often tested in accordance with standards such as BS 7531, or DI N 3535 and ASTM F36, where these standards require testing of material properties such as stress relaxation, compression, recovery and gas permeability amongst others.

Gasket Types

Semi-Metallic

Combination of non-metallic filler for compressibility and metal for strength, resilience and chemical resistance. Used typically at higher temperatures and pressures than non-metallic types.

Spiral-Wound

The **MACER®** range of spiral-wound gaskets are widely used on high pressure joints throughout industry world-wide. These are generally used for higher temperatures and pressures. A variety of metals are available for the winding strip as well as for the support rings. The standard pipeline gaskets are nominally 4.5 mm thick and compressed to a working thickness of 3.2/3.45 mm.

At large diameters (typically over 1.2 metres) then a thicker gasket of 7.3mm thickness is generally used. On raised face flanges, the gaskets have an outer support ring which locates inside the bolt PCD, and they can also be supplied with an inner ring. These are usually for the higher pressure systems, or processes having high flow rates or abrasive media, as the inner ring reduces turbulence at the pipe bore.

On spigot / recess flanges a simple sealing element gasket is usually used with no additional support rings, and the flanges are dimensioned to achieve the .correct gasket compression when metal to metal contact is reached. In these cases the gaskets should be designed having the correct inner and outer clearances for the recess used.

Metal Jacketed

Single and double-jacketed metal clad gaskets have mostly been traditionally used as heat exchanger gaskets. Metals such as soft iron, carbon steel and stainless are used to encase a soft filler material, usually a non asbestos millboard. It should be noted that some heat exchanger flanges have stress raising 'nubbins' on one face, and the non seamed side of a double jacketed gasket is intended to go against this face, so it is important that the joint is fitted the correct way around in the assembly

\leftrightarrow Kammprofiles

The $MACER^{\circledast}$ gasket type is generally a solid metal ring having a serrated tooth form profile on each side. A covering layer of graphite or PTFE is applied, which becomes compressed into the serrated surface when the gasket is loaded. These gaskets have a good level of sealing tightness and are frequently used to replace metal-jacketed joints on heat exchangers. They can also be provided with a slot-leg locating ring as a 'Multi-Fit' design (see Page 35), to reduce stores inventory.

b) Metallic

Manufactured from one metal or a combination of metals in a variety of shapes and sizes for high temperature or pressure use. Due to the high pressures involved, the seating stresses are necessarily large to give sufficient gasket deformation to overcome any flange surface imperfections and to overcome the high system pressure forces.

Oval & Octagonal

These are commonly used on oilfield applications, and details of these joints are given in well recognised standards ASME B 16.20 and API 6A. The gaskets sit in a recess in the flange face, which has 230 angled walls. Some stand-off exists between the flanges, though PTFE inner spacers can be supplied to reduce the effects of erosion and the build-up of dirt on the flange face inside the gasket. Similarly, sponge rubber protectors are sometimes used to keep the area clean outboard of the gaskets and around the bolts. For hydro testing purposes, rubber-covered ring joint gaskets are available, to avoid damaging the flange recesses.

RX & BX

The RX joints are an unequal bevel octagonal ring, and are considered to be α pressure-energised or pressure-assisted seal. The BX is also octagonal, though shorter in profile and designed to go into a recess that comes metal-to-metal when the flanges are tightened. These are used on very high pressure flanges up to 20,000 p.s.i. rating.

Semi-Metallic Gaskets

Gaskets can be manufactured in accordance with all relevant gasket standards to suit the following designations:

- **ASME B16.5**
- **BS1560**
- **BS10**
- · ASME B16.47 SERIES B (API 605)
- · ASME B16.47 SERIES A (MSS-SP 44)
- · BSEN 1092 (BS 4504)
- DIN FLANGES
- **JIS FLANGES**
- **FRENCH NF STANDARD**

Introduction

Semi-metallic gaskets are widely used on the following services:

Steam

repositer handhole, tubecap and manhole assemblies

- ☞ steam and feed water pipe flanges
- **®** feed water heaters
- or valve bonnets
- சை autoclaves

Steam

- **&** catalytic cracking plant
- o vessel closures
- platformers
- [®] line flanges
- Theat exchangers
- a valve bodies

Marine

- o boilers
- o de-aerators
- Reconomisers
- ☞ main feed pumps
- ☞ main steam lines
- **&** LP and HP feed.
- **®** air ejectors
- water heaters
- ☞ diesel engines

Nuclear

- cooling circuit flange (helium and carbon dioxide)
- Thigh temperature gas lines
- o pressure vessels
- **R** valves

Hydraulic

- The high pressure line flanges
- pump and valve bodies

Flange standards

N.B. Gaskets for non standard flanges are also readily available

MACER® Spiral Wound Gaskets

MACER® Kammprofiles **Gaskets**

Metal Jacketed Gaskets

MACER® Spiral wound gaskets

MACER[®] Gaskets are manufactured from V-shaped metal strips, spirally wound with an inlay of filler between each turn. At the start and conclusion of the spiral form, several continuous turns of the metallic windings are securely welded together.

The construction is capable of infinite variety as the number of metal plies in relation to filler plies can be increased or decreased. The metal and filler material can be varied to suit practically any service conditions.

The use of steel supporting rings on the inside or outside of the spiral wound portion (or both) permits the application of **MACER[®]** to be extended to flat or raised face flanges under high pressure lines.

 \ln

identical

produced in a wide variety of shapes, the most common

being circular, obround, square, oval and diamond. The

H/IW incorporates a stainless steel wire on the inner surface which protects in the inner windings and reduces

and vessels.

MACER® Gaskets are manufactured from V-shaped metal strips, spirally wound with an inlay of filler between each turn. At the start and conclusion of the spiral form, several continuous turns of the metallic windings are securely welded together.

- Available in materials capable of withstanding temperatures from the cryogenic range to at least 1000° C
- Can, in standard form, seal pressures up to 350 bar. Higher pressures can be considered on request.
- A Maintain a seal under conditions of thermal cycling or vibration.
- Resist corrosion and leave flange faces clean
- Do not require ground or lapped flange clean.
- Are quick to fit and remove
- Can often be used on bowed or pitted flanges.
- Offer good performance on difficult dry gas or high vacuum applications.

Type C

Type H and H/IW

Basic construction style. Suitable fortongue and groove, male and female or flat face and recess flanges.

these

They can

 C

Type

specifically designed for the

sealing of manholes, hand holes,

tubecaps and plugs in boilers

ore

but

he

appearance

to

Type C/IR

Type SG

Identical to the Type C but fitted with the protective inner ring which gives high pressure and temperature capabilities with improved sealing performance. Used on male and female flanges.

As Type C but fitted with an external ring which accurately centralises the sealing element. In addition the ring provides extra radial strength and acts as a compression stop. Generally used on raised face and flat face flanges.

the risk of extrusion under compression.

Identical to the Type SG but also fitted with an inner ring to prevent damage to the gasket bore and inner windings. It also acts as a heat shield and corrosion barrier and improves recovery characteristics and sealing performance.

Gasket profiles

Type SG/IR

Type TE

This type is identical to the Type C but is fitted with pass-partition bars for use on heat exchangers and vessels. The bars are usually manufactured metal-jacketed gaskets but can also be solid metal faced with graphite, PTFE or soft jointing material.

Type WG and WG/IR

Designed to suit the relatively narrow seating space on many heat exchangers by utilising a spirally wound steel centring ring instead of a solid ring. WG/IR has a solid inner ring.

*whilst we do not generally

recommend above 3550mm.

we have supplied type SG/IR in

excess of 5 metres diameter.

Type WG /TE and WG/IR/TE

Identical to the WG profile but fitted with partition bars. WG/IR/TE has an inner ring.

MACER® manufacturing parameters

The standard MACER® Type SG and SG/IR gaskets are produced with a sealing element thickness of 4.5mm and 3.0mm centring ring/inner rings. However, virtually all types are available in a variety of thicknesses from 2.5mm to 7.3mm nominal. The following tables specify the various nominal and corresponding recommended compressed thicknesses together with maximum and minimum diameters for each thickness

MACER® gasket compression

MACER® gaskets must be compressed by a specific degree if maximum service potential is to be realised.

Note: Due to the compression characteristics of PTFE, full compression may not always be achieved. If flange face contact is essential then special clearances can be considered.

MACER[®] materials

The most widely used material for winding metal is SS 316L and is usually used with carbon steel or stainless steel flanges. The standard inner ring material is also SS 316L. It is normal practice for the inner ring and windings to be the same as, or compatible with, the flange metal. This practice prevents corrosion and differential expansion problems. For very high temperatures or highly corrosive applications, alternative materials may be chosen for both windings and inner rings. PTFE inner rings can be supplied for highly corrosive media.As standard, the centring rings are supplied in carbon steel with an anti corrosion coating/treatment primarily to prevent corrosion in storage. The use of stainless steel for centring rings is quite common where the external flange environment conditions are corrosive to carbon steel, or temperature conditions prohibit the use of carbon steel.

* As standard supplied with a paint coating to inhibit corrosion during storage. Other protective coatings, eg. Zinc plating with a chrome passivate, are available on request.

C

MACER[®] materials

(1) generally applied for the centring ring and ASTM A285-82 GR-C

(2) generally applied for the metal component of the gasket which should be made of non-corroding material

MACER[®] materials

ADVANTAGES OF EXPANDED GRAPHITE AS FILLER MATERIAL:

· Safer to use · Fire safe · No adhesion problems. · Resistance to a wide range of chemicals. · Less effort required to effect seal. · Very versatile. . Best general alternative to compressed asbestos fibre for the majority of applications. . Maximum temperature in steam 65° deg.C. . Inert.

3.2.6 gasket compression. Spiral wound gaskets, NPS 1/2", NPS 3/4" and NPS 1" in classes 150, 300 and 600 shall be designed so that a uniform bolt stress, based on the nominal bolt root diameter, of 25000 psi will compress the gasket to thickness of 0.130 in. +/-0.005 in. All other gasket sizes and classes shall be Designed so that a uniform bolt stress of30000 psi will compress the gasket to a thickness of 0.130 in. +/-0.005 in. The test specified above is a proof test only.

COMPRESSIBILITY & SEALABILITY TEST

MACER® lolode **Spiral wound gaskets**

Some methods of calculation of the bolt load required to compress conventional spiral wound gaskets, result in figures which appear to over - stress the standard bolting of many ASME B16.5 class 150 and some 300 flanges.

Spiral wound gaskets have been used successfully on these flange classes for many years. However a lot more attention has recently been paid to the amount of compression that is actually achieved when standard bolting is employed. The replacement of asbestos with expanded graphite (SPG) filler, has improved this situation by producing equivalent sealing performance under lower compressive forces, as well as allowing greater compression for a given bolt load.

It must be acknowledged that on certain flanges, the amount of available bolting may be insufficient to achieve the degree of compression normally recommended by gasket manufacturers without exceeding the recommended bolt stress levels given in the flange design codes. However, in practice gaskets have been found to be capable of sealing performance especially with class 150 and 300 flanges, even through the gasket may not be fully compressed to the guide ring.

comparison

Typical load-compression

The Lolode gasket has been developed to satisfy those requirements for maximum sealing element compression, using the bolt stress figure of 25,000 p.s.i. given for certain material grades shown in the ASME code. The expanded graphite (SPG) filled **Lolode**, has the basic design and properties of a standard MACER®spiral wound gasket, but it has been carefully engineered to enable compression down to the guide ring under the limited load provided by ASME B16.5 or BS 1560 class 150 or 300 flanges.

Lolode gaskets are available to ASME B16.20 and BS 3381 dimensions to suit class 150 and 300 flanges from 1/2" to 24" nominal bore.

(Note that the large diameter flanges to ASME B16.47 Series A and B do not suffer the same poor ratio of gasket area to bolt area as the smaller flanges such as 3" and 8" class 150, and hence Lolode gaskets are not required for these flanges).

The graph above shows a comparison of the amount of compression obtained at a given gasket stress for the Lolode version compared to a standard MACER® SPG filled spiral wound gasket. It can be seen that the Lolode compresses down to the nominal guide ring thickness of 3.3mm at a significantly lower level of stress than the standard gasket.

$\textit{MACER}^{\circledR}$ Type SG suitable for BS 1560 /ASME B 16.5 flanges - Metric Dimensions

Dimensions in mm

GASKET DIMENSIONS

 $\textbf{MACER}^{\textcircled{\tiny{\textregistered}}}$ Type SG suitable for BS 1560 /ASME B 16.5 flanges – Imperial Dimensions

MACER® Type SG suitable for ASME B16.47 Series A flanges - Metric Dimensions

Dimensions in mm

GASKET DIMENSIONS

$\textit{MACER}^{\circledR}$ Type SG suitable for ASME B16.47 Series A flanges - Imperial Dimensions

 $\textit{MACER}^{\circledR}$ Type SG suitable for ASME B16.47 Series B flanges - Metric Dimensions

Dimensions in mm

GASKET DIMENSIONS

 $\textit{MACER}^{\circledR}$ Type SG suitable for ASME B16.47 Series B flanges - Imperial Dimensions

MACER® Type SG suitable for BS 1560/ASME B16.5 flanges

Dimensions in mm

Up to 40 Bar dimensions in accordance with EN 1514-2

GASKET DIMENSIONS

MACER[®] Type SG suitable for DIN/EN 1092 flanges

MACER® Type SG suitable for BS 10 Welded Neck flanges

 $\textit{MACER}^{\textcircled{\tiny{\textregistered}}}$ Type SG/IR suitable for BS 1560/ ASME B16.5 flanges – Metric Dimension

Dimensions in mm

GASKET DIMENSIONS

 $\textit{MACER}^{\textcircled{\tiny{\textregistered}}}$ Type SG/IR suitable for BS 1560/ ASME B16.5 flanges - Imperial Dimension

Inner Ring Inside Diameters for Spiral Wound Gaskets

USED IN ASME B16.47 SERIES A FLANGES					
Flange Size	Pressure Class				
(NPS)	150	300	400	600	900(1,2)
26	25.75	25.75	26.00	25.50	26.00
28	27.75	27.75	28.00	27.50	28.00
30	29.75	29.75	29.75	29.75	30.25
32	31.75	31.75	32.00	32.00	32.00
34	33.75	33.75	34.00	34.00	34.00
36	35.75	35.75	36.13	36.13	36.25
38	37.75	37.50	37.50	37.50	39.75
40	39.75	39.50	39.38	39.75	41.75
42	41.75	41.50	41.38	42.00	43.75
44	43.75	43.50	43.50	43.75	45.50
46	45.75	45.38	46.00	45.75	48.00
48	47.75	47.63	47.50	48.00	50.00
50	49.75	49.00	49.50	50.00	
52	51.75	52.00	51.50	52.00	
54	53.50	53.25	53.25	54.25	
56	55.50	55.25	55.25	56.25	
58	57.50	57.00	57.25	58.00	
60	59.50	60.00	59.75	60.25	

NOTES:

Dimensions in inches GENERAL NOTES: a . The inner ring thickness shall be 0.117 ins to 0.131 ins b. The inside diameter tolerance is +/-0.12 ins c. Rings are suitable for use with pipe wall 0.38 ins or thicker

1. Inner ring are required for Class 900 gaskets 2. There are no class 900 flanges NPS 50 and larger

GASKET DIMENSIONS

Inner Ring Inside Diameters for Spiral Wound Gaskets

GENERAL NOTES: a. The inner ring thickness shall be 0.117 ins to 0.131 ins b. The inside diameter tolerance is +/- 0.12 ins **Dimensions in inches** c. Rings are suitable for use with pipe wall 0.38 ins or thicker

NOTES:

1. Inner ring are required for Class 900 gaskets 2. There are no class 900 flanges NPS 50 and larger Class 900 flange 3. See pages 22 and 23 for Sealing element and guide ring dimensions.

MACER® Type SGIR suitable for BS 1560/ASME B 16.5 flanges

Dimensions in mm

Up to 40 Bar dimensions in accordance with EN 1514-2

GASKET DIMENSIONS

MACER® Type SGIR suitable for DIN/EN 1092 flanges

MACER[®] Type SG/IR suitable for BS 10 Welded Neck flanges

Dimension in inches

Spiral wound gaskets to ASME B 16.20 can be identified by the colour coding on the outside of the guide ring. The soild colour denotes the grade of winding material, and coloured stripes identify the filler material used.

Gasket profiles

Type CK

Parallel root core for use in confined location including male and female, tongue and groove and recessed flange arrangements.

Type SGK

Parallel root core with integral centring rip_ for correct gasket positioning within the flange bolt circle. Type SG is recommendec for use on standard raised face and flat face flanges.

MACER® Kammprofile gasket

Type LGK

Parallel root core with loose fitting centring ring which reduces the possibility of damage to the core as a result of mechanical and thermal shock.

Kammprofile gaskets consist of a metal core with concentric serrated grooves on each side and the addition of a soft layer of sealing material bonded to each face. Selection of the metallic core material and sealing layer materials is dependent on the service duty.

The serrated metallic core is very effective for sealing in applications where high temperatures, high pressures and fluctuating conditions exist and can be used without sealing layers, but there is a risk of flange damage, especially at high seating load. The sealing layers protect the flange surfaces from damage and also offer excellent sealing properties when supported by the serrated metallic core.

- Can seal pressures up to 250 bar.
- Can withstand temperatures up to 1000°C dependent on core and layer materials used
- · Can maintain effective sealing performance in varying

Advantages

- temperature and pressure conditions.
- Will not damage flange surface and can be removed easily.
- The serrated metallic core can be reused, subject to inspection after clearing and relayering.
- Can be made to suit existing arrangements, without modification.

Gasket materials

MACER ™ gaskets are available to order in a wide variety of component materials

Manufacturing parameters

Normally supplied with a 3.0mm or 4.0mm thick core and covering layers 0.5mm thick, but can also be supplied in other thicknesses.Diameters from 10mm N.B. upwards can be manufactured and the size limitation for each type of MACER™ gasket is as follows:

Type CK up to 5000mm diameter Type SGK up to 2000mm diameter Type LGK up to 2000mm diameter For heat exchanger applications see Page 39 for typical pass partition bar configuration.

Kammprofiles to suit - ASME B16.5/BS 1560 flanges

MACER®gasket dimensions (½"to 24" NSP)

Kammprofiles to suit - ASME B16.47 Series A flanges

Dimensions in mm

MACER® gasket dimensions (above 24" NSP

Dimensions as per Spiral Wound gasket sizes in ASME B16.20, table 10, suit Series A flanges

Kammprofiles to suit - ASME B16.47 Series A flanges continued

Dimensions in mm

MACER® gasket dimensions (above 24" NSP)

Dimensions as per Spiral Wound gasket sizes in ASME B16.20, table 10, suit Series A flanges

Kammprofiles - DIN/BS EN 1092 flanges

Dimensions in mm

MACER® gasket dimensions (above 24" NSP)

Dimensions taken from EN 1514 for EN 1092 flanges

MACER® Multifit gaskets

"One size fits all"

In the most popular piping classes (ASME 150,300,600 & DIN PN 10-100) only ONE gasket is required for each nominal bore size 1/2 through to 24" and 10 NB to 600 NB

User well proven Kammprofile gasket technology with specially designed sealing element and location rings.

The cost effective **Kammprofile**

- Kammprofile consistency & performance.
- Self loading.
- Reduces & simplifies inventory.
- Minimises 'out of stock' risk.
- · Reduces 'lifetime' cost.
- · Re-usable 'clip in' outer guides.
- . Re-usable sealing elements with new facings.
- Full range of materials available.
- Other sizes on application.

How to Order

- Quantity
- . Nominal bore & pressure rating, e.g. 2" 150-600
- Flange description e.g. ASME, DIN
- Material combination e.g. 316L/graphite.

Standard gasket profile

Spiral wound & Kammprofiles gaskets Chemical suitablity guide

347

SS 316, 316L SS 304L 321 **NICKEL VIONEL MET ALLIC COMPONENT** \mathbf{C} \overline{R} METHYLALCOHOL (65°C) Δ Δ Δ A A A \overline{P} A NAPHTHA(20°C) \overline{A} \overline{B} \overline{B} B **NICKEL CHLORIDE SOLUTION (20°C)** A \overline{A} A NICKEL SULPHATE (hot/cold) Λ Δ Δ \overline{A} Δ F F Δ NITRIC ACID (50% @ 20°C) NITRIC ACID (65% @ boiling) B \overline{B} E E D \overline{A} A \overline{A} A OIL - CRUDE (hot/cold) Δ OIL - VEG/MINERAL (hot/cold) Δ \overline{A} Δ Δ Δ D $\mathbf C$ B A B OXALIC ACID (10% boiling) **PHENOL** A \overline{A} \overline{A} Δ $\mathbf c$ \overline{B} \overline{B} \overline{B} \overline{B} PHOSPHORIC ACID (10% @ 20°C) PICRIC ACID (70%) A A \circ \circ \circ POT ASSIUM BICHROMATE (20°C) Δ Δ Δ A A A A POT ASSIUM CHLORIDE (5% boiling) B POT ASSIUM HYDROXIDE (50% boiling) \overline{A} \overline{A} Δ POT ASSIUM NITRATE (5% hot) Δ Δ A Δ \overline{A} A \overline{A} \overline{A} \overline{A} POT ASSIUM SULPHATE (5% hot) **POTASSIUM SULPHIDE (salt)** A A A A Δ Δ Δ Δ **SEA WATER SEW AGE** A Δ Δ \overline{A} Δ SODIUM CARBONATE (5%@ 65°C) $\overline{\mathsf{A}}$ \overline{A} A A A \overline{B} \overline{B} \mathbf{C} \mathbf{C} SODIUM CHLORIDE (saturated/boiling) Δ Δ Δ Δ **SODIUM HYDROXIDE** Δ Δ **SODIUM HYPOCHLORITE (5% still)** B $\mathbf c$ $\mathbf c$ $\mathbf C$ $\mathbf c$ **SODIUM NITRATE (fused)** R Δ B Δ SODIUM SULPHATE (20°C) \overline{A} Δ \overline{A} \overline{A} \overline{A} B D \mathbf{C} \mathbf{C} SULPHUR DIOXIDE (MOIST 20°C) A **SULPHUR (WET)** \overline{B} \overline{B} R \overline{A} Δ $\mathbf C$ **R B** $\mathbf C$ Δ SULPHURIC ACID (10% @ 20°C) SULPHURIC ACID (fuming @20°C) $\mathbf c$ \overline{B} \mathbf{C} \overline{B} \overline{B} \mathbf{c} F \overline{R} F F SULPHUROUS ACID (saturated 190°C) \overline{A} \overline{A} \overline{A} \overline{A} A TANNIC ACID (65°C) E $\mathsf E$ \overline{B} \overline{B} \overline{B} **TRICHLORACETIC ACID (20°C)** B **B** \overline{B} B B ZINC CHLORIDE (5% boiling) A \overline{A} A \overline{A} A ZINC SULPHATE (25% Boiling)

200
400

625

VCONEL

Notation:

- A Fully resistant (less than 0.009mm penetration per month)
- \overline{B} Satisfactory (0.009mm - 0.09mm per month)
- C Fairly resistant (0.09mm - 0.025mm per month)
- Slightly resistant (0.25mm 0.9mm per month) D

Non-resistant (over 0.9mm per month)O Insufficient data available E Where chemical compatibility is not indicated, or a chemical is not listed, please consult our technical services team for a recommendation to be made

Due to the complexity of making a recommendation for any given duty, this section on chemical compatibility is intended only as a guide. The possible effect of elevated temperatures should be considered when determining the compatibility of these products with a chemical. If necessary, please contact our technical services team for assistance.

Filler and facing materials:

EXPANDED See details for Supagraph Plain Sheet **GRAPHITE:** HTF (HIGH When used with suitable winding steel grades, this material

TEMPERATURE resists the majority of common media including; hot oil, fuels, FILLER): acid, alcohols and esters. It should NOT be used with sulphuric, phosphoric, hydrofluoric or other strong mineral acids.

PTFE (WITH 25% This material is chemical inert to most media, with a few **GLASS FIBRE):** exceptions as follows :-It offers only fair resistance to : ammonium hydroxide, bromine, chromic

> acid, hydroboric acid, hydrochloric acid, hydrocyanic acid, nitric acid (0.50%), phenol and sodium hydroxide

It should NOT be used with :- fluorosilicic acid, hydrofluric acid, hydrogen sulphide solution or sodium silicate.

Metal jacketed gaskets

These gaskets are specially designed and widely used for heat exchangers, autoclaves, columns, pressure vessels, flue stacks, boilers, gas mains, valve bonnets, pumps and similar services.

The gaskets are manufactured from a soft, pliable filler core surrounded by a metal jacket chemically and thermally resistant to the working conditions, which may totally or partially enclose the filler.

The majority of these types of gasket are supplied in circular form but can be manufactured to other shapes to suit individual requirements. The method of manufacture enables gaskets to be produced with almost no size limitation. They are produced in different styles to API, ASME, DIN and BS standards.

Metal jacketed gaskets are frequently required with pass partition bars, which may be manufactured by two methods, either with 'integral' bars or with bars welded onto the main gasket. Both methods have advantages and we are able to supply to either method of construction.

Integral bars

This method of construction ensures that the gaskets have uniform hardness around the main periphery of the primary seal and along the pass partition bars. As there is a solid join between the bars and the main gasket, the construction is more robust and eliminates the possibility of seepage of the media into the core of the gasket. This construction is recommended for the sealing of hazardous fluids. We recommend that this style has at least a 10mm radius at all intersections, this maintains a continuous metal overlap, which prevents splitting of the metal.

Welded bars

This method of construction has distinct commercial advantages as it allows full material utilisation. Welding is carried out using methods which ensure that metal hardening is minimized.

Flange nubbins

Flange nubbins are often used to increase stress and in such cases, care must be taken to install the gaskets with the seamed face on the opposite side.

The gasket seam should be on the opposite side to any fange nubbin (s)

Metal jacketed gasket Styles

M120 Single jacketed Soft filler - open type

M123 Double jacketed Soft filler - totally enclosed

Metal jacketed gasket materials

Metal Jacket

Metals are only used in the annealed condition and limit the hardness of the metal in line with international standards as shown.

Fillers

Selection of the correct filler is important and as standard we use a soft non-asbestos filler. This material is constructed from inorganic fibre and inert fillers, suitably bonded, which produces a material having very similar characteristics to those of asbestos millboard. A data sheet on this material is available on request. Alternative fillers include expanded graphite, PTFE & compressed non-asbestos fibre.

Metal Jacketed Gaskets Kammprofile Gaskets **Spiral Wound Gaskets**

Heat Exchanger gasket shapes

- Typical pass partition bar configurations

MACER® Metal ring joint gaskets

Protection

Soft iron and low carbon steel ring joint gaskets to API Standard 6A are supplied with zinc plating to 0.0002" -0.0005" thick unless otherwise specified. Other platings are also available, if preferred. Unplated rings are treated with a rust preventive fluid.

During storage and handling it is very important that the mating faces (the oval radius or the chamfered face) are not damaged as this can lead to leakage when the ring joint is used in its particular application.

To afford the maximum degree of protection, MACER offer as an extra feature individual vacuum packaging. Gaskets are vacuum packed using a strong clear film onto a stout backing board. This style of packaging ensures full protection of the gasket, whilst allowing visual inspection of its condition and marking.

Materials

Gasket metal should be selected to suit the service conditions and should be of a hardness lower than the flange metal. At MACER, the annealing process of the metal and the machining is carefully controlled to keep the hardness of the gasket below the maximum allowable, to ensure correct flow and sealing without damage to the flange surfaces. Checks carried out during manufacture ensure that the hardness of the finished product does not exceed the figures stated below.

The styles described are manufactured as standard and are available ex-stock or to short leadtimes. When ordering please submit the following data:

- Gasket standard.
- Relevant ring number or nominal pipe size with rating.
- Material required.
- Oval or octagonal shape for style "R" gaskets.
- Quantity and required delivery.

The principal types of material are:

Other stainless and super alloy steels, Duplex, Monel, Inconel, Incoloy, Nickel other materials are available. Based on almost 50 years of experience, Moorflex have established specifications to ensure gasket suitability. Certification and compliance with NACE MR0175 are standard features

Identification and traceability

For convenience in ordering, numbers are assigned to gaskets and prefixed by the letter 'R','AX' or 'BX', followed by the material identification. Marking is effected so as not to injure the contact faces, nor to harmfully distort the gasket. MACER use only low stress DOT stamps approved to NACE standards in order to ensure that stresses are not introduced into the gasket.

All non-API gaskets are typically marked MACER R45 S316. Gaskets complying to API Standard 6A are additionally marked with API Monogram Licence No., Product Specification Level 4 and date of manufacture. (It is standard procedure for MACER to supply API 6A gaskets to PSL4) All API gaskets are typically marked:-MACER 6A-0038 R45 S316-412/2001 (December 2001).

Traceability of material and constant monitoring of manufacture are essential for effective quality control. All MACER ring joint gaskets carry a Material Reference **Number**, which directly relates to the batch of material from which it was manufactured The MRN number is applied to the gasket in the same way as the identification marks. This reference is included in material certificates, thus ensuring full traceability of supply.

Series 'R' manufactured to the standards

ASME B 16.20 - API Std 6A BS EN 12560-5

All dimensions are in inches. denotes API Std. 6ARing Joint gaskets.

Gasket styles and types

Series 'R' Octagonal

The type R oval configuration is the original ring joint design and was followed by the type R octagonal which offered more specific sealing contact areas. Both types can be used with flanges having the standard ring joint flat bottom groove and hold off flanges by a specified amount, relying entirely on correctly applied initial bolt-load for their proper operation in service.

Available in ring numbers R11 through R105 to suit the following flange specifications.

ANN

All dimensions are in inches. denotes API Std. 6ARing Joint gaskets.

Series 'RX'

As well-head pressures increased to 700 bar (10,000lbf/in²) and beyond, flanges designed with type 'R' oval or octagonal rings became excessively heavy, requiring impracticably large bolts to perform the

double duty of holding pressure while keeping the gasket compact.The solution to this problem was found inhigher strength materials and the development of the 'RX' and 'BX' series joint which are pressure energised. (The higher the contained pressure, the tighter the seal). The 'RX' Style Ring Joint has the unique self-sealing action. The outside bevels of the ring make the initial contact with the groove as the flanges are brought together,

thus pre-loading the gasket against the grooved outer surfaces. Internal pressure during service increases this loading and, therefore, the gasket's sealing performance. Available in ring numbers RX20 through RX215 to suit the following flange specifications:

Series 'RX' manufactured to the standards **ASME B 16.20 - API Std 6A**

All dimensions are in inches. ^ Denotes API Std. 6A Ring Joint Gaskets.

Style 'BX' Ring joint Gaskets can only be used with special 'BX' grooves and are not interchangeable with the Style 'RX' series.

Designed to API specifications for use with grooved flanges on special applications involving high pressure up to 20,000 p.s.i. the 'BX' series is available in ring numbers BX 150 through BX 303 to suit the following flange specifications:

Series 'BX'

Series 'BX' manufactured to the standards **ASME B 16.20 - API Std 6A**

Calculation Methods

As stated in section 2, the load-sealability characteristics of a gasket are quite complex. Incorporating these effects into a reliable flange design method has been the objective of designers for many years, and a number of flange design codes are now well recognised. The ASME VIII and DIN 2505 codes are well established and successfully in use. However, certain limitations in these codes have lead to research and development of alternatives, such as the PVRC and CEN methods. Macer recognises both the merits and limitations of all the methods which have been summarised and commented upon in the following paragraphs. Individual design parameters will dictate the most appropriate method and for further advice on gasket selection and relevant load sealability requirements, please contact our technical specialists.

a ASME VIII

The ASME code has been used for many years to design flanges, though has a number of recognised flaws when it comes to determining a suitable bolt load with regard to gasket sealing. Calculations are performed to determine greater of either the operating or initial forces using the following formulae.

The factors 'm' and 'y' are the 'gasket factor' and initial seating stress values respectively. One problem is that the code does not utilise the whole gasket contact area in the calculation. In the formulae above, the "effective width" is 'b' and the "effective diameter" is 'G'. The system pressure is designated as 'P' in these equations. If we consider a common raised-face flange, then the contact width of the gasket element (from the raised face outside diameter to the gasket inside diameter) is designated as 'N'. The basic width is then calculated as being 1/2 this value and called b The "effective width" Othen depends upon the value of be being greater or less than 1/4", though in the majority of cases this is likely. If b is Ogreater than 1/4", then the effective width is calculated as:-

(Or for cases where b_n is equal or less than 1/4", then $b = b_n$) OThe effective diameter 'G' is simply the outside contact diameter less 2 x b_o Therefore, the actual gasket contact area is usually far greater in reality that the calculated figure by this method. Note also that the gasket factor 'm' is effectively a multiplier of the system pressure as an operating stress. However as shown in section 2, the actual sealing performance of a gasket is more realistically a 3 dimensional, exponential decay curve, rather than a single number.

Again, as per section 2, we know that it is the operational stress that defines gasket sealability. There seems to be no real reason to try and link initial gasket seating loads (i.e. for compression purposes, to take up flange flatness etc.) with the 'm' factor which is related to the operating stress requirement for a given system pressure. However, when originally devised in the 1930's and 1940's, the relationship existed between the factors of :-

$(2m-1)$ X 180 = y

(using y in units of p.s.i, and rounding-off the m factor to the nearest 0.25) Thus, for compressed fibre gaskets, a lower y value was determined for the thicker materials, presumably because they would deform more readily to make a crude seal against whatever flange distortion existed. Thus, from the relationship above, the thicker materials also gained a lower m factor, suggesting that they -would give better sealing performance. However, again as per section 2 of this manual we know that thicker materials not only have a greater tendency to stress-relax, but also have a greater number of micro-porosity channels where leakage can occur. Indeed, in searching gas sealability tests, then a 3 mm, thick compressed fibre jointing material tends to leak at approximately twice the rate of a 1.5 mm sample of the same material at a given operating stress.

a ASME VIII

This method also employs gasket factors that are used to determine the bolt load requirement. There are the maximum and minimum stress levels for installation at ambient temperature, as well as a maximum stress at elevated temperature

The maximum initial gasket stress allowable is a function of the width to thickness ratio to avoid crushing effects on soft materials. This method also has an 'm' factor, though uses the actual contact width of the gasket in the calculations. Thus, this method is less likely to produce insufficient gasket stressthan by ASME VIII, especially as the minimum initial gasket stress values given in the code are fairly conservative.

Another popular European design method used to determine bolt load requirements is the AD-Merkblatt B7, where again the initial and operating bolt load requirements are determined using gasket factors. These are kl, k0 and KD, which relate to the effective widths and deformation resistance of the gaskets concerned.Note that both of the above methods are now generally tending to .be replaced by the new EN 1591 design method.

c PVRC

For a number of years the Pressure Vessel Research Council has recognised some of the inadequacies of the ASME code andsought to provide a better means of calculating the required gasket loading. The proposed calculation requires gasket data to be developed from a series of loading and unloading leak tightness tests in order to obtain coefficients to describe the sealing performance of the gasket. This method uses the concept of 'Tightness Parameter', where the gasket sealability is related to a dimensionless number thus:

This formula essentially relates the test pressure to atmospheric pressure, and the measured leak rate against a unitary leak rate measured in mg/sec/mm diameter of gasket. The index of 0.5 suggests that doubling the system pressure will in fact produce a fourfold increase in leak rate, though this is perhaps a worst-case scenario for most gaskets. The coefficients used in the calculation are G, a, and G and are derived from the b ssealablility test as shown in the Typical PVRC Chart.

There is some debate about the reliability and repeatability of the coefficients as they are derived from the log-log plot of an assumed square-law relationship, so relatively minor changes in leak rate during the test could affect the final data reduction.

However, the coefficients are at least derived from actual tightness testing, so the calculation becomes realistic in terms of typical in-service performance of the gasket.

d CEN

Like the PVRC method, this uses loadingunloading gasket sealing tests to determine the gasket performance characteristics. They are used in a flange calculation method (EN1591) which is quite iterative and complex in nature. As a gasket is loaded, some flange rotation may occur, changing the effective stress on the gasket from the inside to outside contact position (as described previously in section 1). The gasket seals differently in the unloading phase of the test compared to the loading cycle. If we consider that a gasket is loaded to point Q initially, and Aunloaded by the hydrostatic to the operating stress Q as shown in the SminLdiagram below, then we can see that the sealability decreases slightly between these two points. However, the sealability is generally better than when this stress level was applied during the loading phase.

As mentioned in section I, the unloading modulus of the gasket changes with increased initial stress. Therefore, the change in sealability between QA and Q_{sminL}will change depending upon the actual

value of Q applied. This standard uses Athe unloading modulus of the gasket in the calculations to examine the stiffness of the gasket as a part of the overall joint stiffness. The EN 1591 method looks at the required sealability from loading-unloading tests. By knowing the degree of unloading on the joint from the hydrostaticforces and the tightness level desired, it is possible to calculate the flange deflection and effective gasket stress for a given bolt load. Therefore, changes to the flange geometry and' applied bolt load will determine the amount of flange rotation, the change in gasket stress across the sealing element, both in the initial and operating conditions, and therefore the

degree of tightness achieved. The problem with this method is that it can be quite iterative and complex, though computer programmes are becoming available which will make the calculation method easier to perform.

The degree of gasket testing required can also be considerable, and work is underway to look at combining the methodologies of both the CEN and PVRC testing to harmonise the test protocols.

GASKET STRESS

Best Practice

(A) Do's and Don'ts

- Mating flanges should be of the same type and correctly aligned.
- Fasteners should be selected to ensure that they do not exceed their elastic limit at the required tension.
- \bullet Do not re-torque elastomer bound compressed non-asbestos gaskets after exposure to elevated temperatures (they may well have hardened and are at risk of cracking).
- **T** Ensure that fasteners show no signs of corrosion, which might affect their load bearing capacity.
- V Nuts should have a specified proof load 20% greater than the UTS of the fastener.
- Hardened steel washers of the same material as the nuts should always be used.
- A thread lubricant or anti galling compound should be used on bolting as appropriate, but only a thin uniform coating should be applied. Where stainless steel is used, it should be ensured that such coating are suitable for use.
- A thread lubricant or anti galling compound should be used on bolting as appropriate, but only a thin uniform coating should be applied. Where stainless steel is used, it should be ensured that such coating are suitable for use.
- Fasteners and/or gasket should never be re-used.
- Good quality gasket should always be procured from reputable suppliers only.
- Gasket should be kept as thin as possible.
- Gasket should never be hammered out against the flange, it will also damage the aasket and thereby reduce aasket performance.
- When cutting full-face gaskets, the bolt holes should be cut first, followed by the gasket outer and inner diameters. Note that if the bolt holes are fairly close to the gasket O/D , then punching out the holes last may produce enough street to crack the gasket at this point.
- Gasket should be stored in a cool dry place, away from heat humidity, direct sunlight, ozone sources, water, oil and chemicals.
- They should also be stored flat (i.e. not hung on hooks).
- Avoid the use of Jointing compounds and pastes. These can lubricate the flange gasket interface and encourage stress relaxation effects.

Gasket Installation

(B) Bolt Tightening

Gasket should be tightened evenly in at least three, or even four stages using an opposed-pattern as illustrated here. Be aware that "crosstalk " exists between

tightens and the gasket compresses, another boit may loosen. Therefore, a final pass around all of the bolts at the end is suggested to ensure that all remain tight.

Bolting

Having determined the gasket loading requirement, consideration must be given to the best materials and tightening methods to achieve this loading. As mentioned previously the overall joint integrity is essentially a function of three main criteria: Correct gasket selection to suit the operating conditions and the overall bolted joint strength / stiffness. Quality of the joint components - the gasket manufacture, flange and bolt materials, etc. Installation competence - ensuring that the gasket is fitted correctly, with the design seating stress applied both accurately and evenly.

(A) Materials

Commonly used bolting materials and standards include BS 4882 and ASTM A 193.It should be noted that stainless fasteners (e.g. "B8") have a significantly Jower strength than alloy steel materials ("B7"). Care should be taken to select a bolt material having sufficient yield strength so as to be able to apply adequate gasket stress whilst retaining a margin of safety, bearing in mind the. variance of torque tension scatter that may be possible during tightening. Note also, that especially with some exotic bolt materials and at elevated temperatures, the true onset of yield may be below the theoretical value. Bolt material standards such as those mentioned above should be consulted for details of maximum recommended stresses and operating temperatures.

Simplified Formula

 \mathbf{L}

In simplified form, for lubricated fasteners, washers, nuts etc, the approximate relationship between torque and fastener may be represented as:

Torque = 0.2 x Load x Diameter

Obviously, the units used must be consistent with the system being used (for example if torque is required in ft-Ibs, then for bolts in inches, the value must be divided by 12 etc.). Compared to the more complex formula given above, then the simplified formula shown here is often deemed sufficient for purpose, as accurately gauging the coefficient of friction can be extremely difficult. However - please note that the accuracy of applied torque vs. actual fastener tension achieved, can be typically +/- 60%.

The effect of the friction coefficient on the variance of the torque-tension relationship can readily be seen on the following graph.

Here we use a nominal 0.15 as being the friction both on the thread and on the nut washer interface on a conventional UNC threaded fastener. Using the more complex formula given above, we can see that a change of only + 0.05 on the friction coefficient can vary the torque required by typically 30%

(B) Tightening Methods

Torque vs. Tension

Whilst torque is often recommended as a method for loading bolts in order to achieve a reasonable gasket stress, it should be noted that because of the variance in nut and thread friction which is particularly difficult to control, then the theoretical relationship is not particularly accurate. Here, F is the axial load requirement, A is the across-flats dimension of the nut (i.e. the outside diameter of nut and washer contact), and D is the washer inside diameter. The friction coefficients under the head of the nut, and on the thread (μ, μ) will h talmost certainly be difficult to determine. The effective diameter (d) , the epitch of the threads (p) , and half the thread form angle (0), are all readily available in engineering manuals for common thread forms.

Hydraulic Tensioning

Hydraulic tensioners have a number of advantages when it comes to tightening large bolts in particular, and can provide significant amounts of tightening power. They offer the ability to be linked together, so that a number of bolts may be tightened in unison. However, some compliance exists in the tensioner system (e.g. embedding of the nut and washer, and thread deflection etc.), so that some overload is required to compensate for the relaxation once the tensioner has been de-pressurised. The degree of torque imparted to the nut collar when the nut is 'run-down' the fastener: also has an effect on the amount of load-transfer relaxation that occurs when the tensioner is de-pressurised.

Bolting Data for ASME B16.5

FLANGE DIMENSIONS

Bolting Data for ASME B16.5

Bolting Data for ASME B16.5

FLANGE DIMENSIONS

Bolting Data for DIN/EN 1092

Bolting Data for DIN/EN 1092

FLANGE DIMENSIONS

Bolting Data for BS 10

Bolting Data for BS 10

FLANGE DIMENSIONS

Bolting Data for BS 10

THREAD DIMENSIONS

Bolting - UNC/UNF:

THREAD DIMENSIONS

Bolting - BSW/BSF

Conversion factors:

Temperatures:

THREAD DIMENSIONS
Bolting - Metric

Metallic Materials

Information in this publication and otherwise supplied to users is based on our general experience and is given in good faith, but because of factors which are outside our knowledge and control and affect the use of products, no warranty is given or implied with respect to such information. Specifications are subject to change without notice. Statements of operating limits quoted in this publication are not an indication that these values can be simultaneously applied

HEALTH WARNING:

If PTFE (e.g. Fluolion) products are heated to elevated temperatures, fumes will be produced which may give unpleasant effects, if inhaled. Whilst some fumes are emitted below 300°C, the effect at these temperatures is negligible Care should be taken to avoid contaminating tobacco with PTFE particles or dispersion which may remain on hands or clothing. Health & Safety data sheets are available on request.

Worldwide equivalents for stainless steel materials:

Material

Colour

Bolt Material Strengths:

Ring Joint Gasket Metals

Spiral wound gaskets to ASME B16.20 can be identified by the colour coding on the outside of the guide ring. The soild colour denotes the grade of winding material, and coloured stripes identify the filler material used.

Notes :- $1)$

Proof loads for stainless steels and "B" grades are approximate values and based upon experience.

Notes :- $2)$

Maximum bolt stresses for "B" and "A" grades are specified in BS 4882 and BS 6105 Values for the stainless steels (e.g. B8 and the "A" grades) must be adhered to. The "B" grade low alloy steels can safely be loaded to the values listed above.

Notes :- $3)$

The maximum values for the "B" steels (except B8) and ISO steels are based upon approximately 85% of the listed proof load, as the true onset of yield can often be detected at a slightly lower than theoretical stress point.

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